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TITLE

REACTIVE PERSONNEL PROTECTION SYSTEM

INVENTORS

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BACKGROUND OF THE INVENTION

1. FIELD OF THE INVENTION

This invention relates generally to the field of apparatus and methods for shielding the body from hostile gunshot activity or bomb explosions. More particularly, this invention relates to an apparatus and method for the automated introduction of a protective, inflatable shield between the concussive force of a bomb blast or the impact energy of a projectile, and the body of the person at which it is directed.

2. DESCRIPTION OF THE RELATED ART

Many different approaches to the protection of personnel from life-threatening attacks exist. Examples of such approaches include bullet-proof glass, concrete and steel building structures, armored cars, bullet-proof jackets, and others. The particular avenue taken depends on whether the person is stationary, located in a vehicle, located within a building, or is required to maintain mobility outside the confines of any specific stationary structure.

Many law enforcement agencies have the designated task of protecting public figures from terroristic attacks. Most often this protection is achieved through some combination of passive personnel armor (e.g., previously mentioned bullet-proof vests, etc.), identification and control of potential sniper vantage points, and passive protection such as shields, bullet-proof glass, armor plates, and other devices mentioned previously. Since public

1 figures often desire unrestricted access to the public and
2 commensurate high visibility, traditional ballistic screens and
3 placement of protective personnel in close proximity are often not
4 practical or effective. Therefore, a need exists for an
5 unobtrusive, reactive device that provides adequate ballistic
6 protection. This need can be satisfied by detecting an incoming
7 pistol or rifle ballistic projectile, discriminating that
8 projectile from other potential airborne particles or objects, and
9 activation/deployment of a protective device, prior to the arrival
10 of the projectile at the designated target.

11 A search of the prior art did not disclose any patents that
12 read directly on the claims of the instant invention, however, the
13 following U.S. patents were considered related:
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18 1,0030+
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PATENT NO.	INVENTOR	ISSUE DATE
3,861,710	Okubo	January 21, 1975
4,856,436	Campbell	August 15, 1989
5,327,811	Price et al.	July 12, 1994
4,782,735	Mui et al.	November 8, 1988

21 **Okubo** discloses a vehicular safety system having an obstacle
22 detector and an impact detector. These detectors are coupled to a
23 single, inflatable air bag which can be deployed by the activity of
24 either detector. One of the detectors is a Doppler radar for
25 predicting collision with the vehicle, and the other senses impact
26 at the moment it occurs between the vehicle and another object.
27 The air bag is incrementally inflated by signals emanating from

1 either of these detectors, being interposed between the occupants
2 of the vehicle and destructive interior vehicle surfaces.

3 **Campbell** discloses an invention to automatically cover
4 electronic equipment for protection from automatic sprinkler
5 systems and other sources of water during the activation of a fire
6 alarm. The cover is deployed by the automatic expansion of spring-
7 loaded telescopic arms which respond to a manual or electronic
8 alarm signal. The cover can be manually reset by rotating and
9 compressing the telescopic arm system to replace the cover into its
10 enclosure. The object of this invention is to protect expensive
11 equipment from fire, smoke, and water damage resulting from fire in
12 the immediate vicinity of the equipment.

13 **Price et al.** describes an adaptable bullet-proof vest which
14 makes use of SPECTRA® materials components. The body armor vest
15 consists of several pieces of SPECTRA SHIELD® material (consisting
16 of resin bonded fibers) sewn into woven ballistic SPECTRA® fiber
17 fabric. This combination of woven and non-woven SPECTRA®
18 components creates increased levels of protection for a bullet-
19 proof vest, while simultaneously reducing weight and bulk.

20 Finally, **Mui et al.** speaks to a bullet-proof protection
21 apparatus consisting of a full-length, inflatable body shield which
22 can be carried in a portable fashion. The shield consists of an
23 encased, inflatable mattress which is deployed by manual activation
24 of a pressurized gas source. This invention anticipates the use,
25 storage, and re-use of the mattress.

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1 SUMMARY OF THE INVENTION

2 Public officials, military personnel, and civilian leaders are
3 often exposed to a wide range of physical threats. While the
4 related devices described in the previous section are somewhat
5 effective in detecting destructive terroristic activity, each
6 approach has its own limitations. The most likely threat areas
7 currently encountered are those provided by high explosives,
8 detonated within a building or at some short distance from a
9 building, and small arms fire (e.g. an assassination attempt). The
10 invention herein described incorporates a combination of systems to
11 produce a robust, unobtrusive, and easily installed apparatus which
12 acts to defeat these threats after detonation of a bomb, or
13 discharge of a weapon.

14 The present invention is a reactive personnel protection
15 system which acts by detecting the presence of a destructive force
16 or object and interposing a protective shield between personnel
17 under attack and the force in an almost instantaneous fashion.
18 Several embodiments of the invention are provided, namely,
19 detection of an incoming small arms projectile, or detection of a
20 concussive blast triggered by a bomb explosion. In either case, a
21 triggering mechanism is provided to rapidly inflate an air bag
22 fabricated from SPECTRA®, KEVLAR®, or similar materials. This air
23 bag is rapidly inflated and interposed between the projectile or
24 concussive force and the person to be protected so as to either
25 deflect the projectile or reduce the effects of the concussive

1 force.

2 In the case of projectile detection and protection, a radar-
3 based bullet detection system with anti-jamming electronics is used
4 to detect the presence of an incoming small arms projectile and
5 determine its path of travel. A bi-static radar system is used to
6 detect the Doppler shift signature of any detected objects to
7 reliably determine the presence of a bullet, and discriminate
8 between the bullet and any other rapidly moving object in the
9 vicinity. Additionally, signal processing circuitry and algorithms
10 are used to help differentiate between projectiles and noise or
11 other extraneous signals to prevent false alarms. Once the
12 presence of a ballistic object is confirmed, a control unit
13 activates a gas generation device, which in turn rapidly inflates
14 an anti-ballistic air bag.

15 In the case of a concussive blast triggered by a bomb
16 explosion, the detection mechanism consists of blast pressure
17 gauges or other devices which are sensitive to rapid changes in
18 acceleration (if mounted to a physical structure), and/or air
19 pressure (e.g. the concussive wave front which accompanies an
20 explosion). These blast pressure gauges are placed at a suitable
21 distance from, and on a periphery around, the personnel to be
22 protected. Other devices, such as magnetostrictive transducers,
23 ultrasonic transducers, accelerometers, and other mechanical and/or
24 electro-mechanical sensors can also be applied to sense the
25 occurrence of a concussive explosion. Signal analysis hardware is

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1 used to discriminate and verify the presence of a concussive blast
2 wave front. Redundant verification is also provided, to minimize
3 the likelihood of accidental deployment. Further, anti-jamming
4 electronics are used to provide immunity to electronic noise which
5 may otherwise render the system inoperable. Of course, such
6 redundant verification and anti-jamming electronic systems are also
7 applied to the aforementioned ballistic object detection system.

8 In the case of either detection system, any type of
9 destructive force confirmation signal resulting therefrom is used
10 to bring about the rapid inflation of an anti-ballistic air bag.
11 This air bag is specially fabricated from ultra-high molecular
12 weight polyethylene, such as SPECTRA®, KEVLAR®, or similar
13 materials which can be used to redirect or lessen the approach of
14 an unwanted destructive object or force. The overall size of the
15 inflated bag depends upon the desired level of protection and the
16 time needed to deploy the bag. Vents are incorporated into the bag
17 to control stress in the bag material during deployment, and also
18 to determine the length of deployment time. Prior to deployment,
19 the air bag is housed in an unobtrusive container having a metallic
20 base plate, and held in place with a pinching bar. The container
21 has a frangible surface through which the air bag can be rapidly
22 deployed.

23 A gas generation system (also housed in the container holding
24 the air bag) is used to fill and deploy the anti-ballistic air bag.
25 Multiple air bags and/or multiple generators may also be employed,

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1 depending on the particular system protection requirements.

2 It should be noted that the present invention is distinctly
3 different from existing sniper detection systems, which are
4 designed to locate the source of a ballistic projectile after the
5 target has been hit, so that return fire or other offensive actions
6 can be taken. These systems typically make use of Doppler radar or
7 acoustic technology, and do not incorporate any proactive,
8 protective capabilities. The present invention, however, is
9 designed to detect the presence of the projectile during its
10 flight, and before impact.

11 Therefore, the reactive personnel protection system of the
12 present invention makes use of a radar-based bullet detection
13 system, or a concussive blast detection system, which provides an
14 inflation signal to an anti-ballistic air bag interposed between
15 the approach of an unwanted destructive object and the personnel to
16 be protected. The signal denoting approach of a destructive force
17 is analyzed and confirmed to make sure that it is properly
18 differentiated from noise or other extraneous signals which may be
19 present. The detection system further includes anti-jamming
20 circuitry for electronic noise immunity and redundant verification
21 to help prevent spurious activation of the air bag.

22 **BRIEF DESCRIPTION OF THE DRAWINGS**

23 Fig. 1A is a perspective view of the explosion protection
24 embodiment of the present invention before air bag deployment.
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1 Fig. 1B is a perspective view of the explosion protection
2 embodiment of the present invention after detection of an
3 explosion.

4 Fig. 2A is a perspective view of the ballistic protection
5 embodiment of the present invention before air bag deployment.

6 Fig. 2B is a perspective view of the ballistic protection
7 embodiment of the present invention after detection of a ballistic
8 projectile.

9 Fig. 3 is a three-view depiction of a deployed air bag.

10 Fig. 4 is a schematic block diagram of a bi-static radar
11 ballistic projectile detection system.

12 Fig. 5 is a schematic diagram for Doppler-shifted tone
13 detection.

14 Fig. 6 is a schematic diagram of a gas-generator squib
15 ignition circuit.

16 DETAILED DESCRIPTION OF THE INVENTION

17 Turning now to Fig. 1A, a perspective view of the explosion
18 protection embodiment of the present invention can be seen. This
19 view depicts the state of the apparatus of the present invention
20 prior to detection of a concussive (blast) pressure wave. Person
21 (100) is shown seated in a room (90) having doorway opening (80).
22 Pressure wave sensor (50) is placed at some distance away from air
23 bag enclosure (20) sufficient to ensure that pressure wave (70)
24 emanating from explosion (60) will not reach person (100) before
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1 the protective element of reactive personnel protection system (10)
2 can be fully activated.

3 Referring now to Fig. 1B, the deployed condition of the
4 present invention can be seen. Since sound normally travels at a
5 speed of 1,025 ft./sec. at sea level, and it may take air bag (25)
6 approximately 30 msec. to deploy, the minimum distance that sensor
7 (50) should be placed from enclosure (20), which houses air bag
8 (25), is 50 ft. This gives approximately 20 msec. for the control
9 unit (40) to process the signal provided by sensor (50) via sensor
10 output conduit (55), confirm that the signal indicates the presence
11 of a destructive pressure wave (70), and initiate deployment of air
12 bag (25) via trigger output (30).

13 Turning now to Fig. 2A, a perspective view of the ballistic
14 protection embodiment of the present invention before the
15 protective element has been deployed can be seen. It has been
16 determined that the best method for detecting the presence of a
17 bullet (130) is radar technology; acoustic-based systems are less
18 reliable and can be defeated by silencers applied to small arms.
19 Doppler radar systems have been used successfully as velocimeters
20 in ballistic applications, and in general, Doppler radar system
21 perform well in noisy and/or geometrically complex environments.
22 The present invention incorporates a bi-static configuration of
23 Doppler radar in which a separate illuminator or transmitter (110)
24 is located at some distance from passive receiver (120). The
25 sensor output conduit (55) from receiver (120) is monitored by

1 control unit (40) and, after suitable analysis and discrimination,
2 trigger output (30) is activated whenever the presence of bullet
3 (130) is detected and confirmed. Trigger output (30) is sent to
4 enclosure (20), which houses air bag (25) (not shown in this
5 figure).

6 Turning now to Fig. 2B, the deployed condition of the
7 ballistic protection embodiment of the present invention can be
8 seen. Initial trajectory (140) of bullet (130) has been detected
9 by receiver (120) and air bag (25) has been deployed from enclosure
10 (20). It should be noted that several enclosures (20), housing
11 multiple air bags (25), can also be employed in this embodiment of
12 the invention. Once control unit (40) has determined initial
13 trajectory (140) of bullet (130), then the appropriate air bag (25)
14 can be deployed via trigger output (30). This figure also
15 illustrates intermediate trajectory (150) of bullet (130), after it
16 is redirected by encountering front surface (220) of air bag (25).
17 Bullet (130) is further redirected by rear surface (230) to follow
18 exit trajectory (160). As mentioned previously, air bag (25) is
19 deployed by control unit (40) so as to interpose a protective
20 shield between the initial trajectory (140) of bullet (130) and
21 person (100).

22 Lightweight materials, such as DuPont's KEVLAR® and Allied
23 Signal's SPECTRA®, are available as woven fabrics to provide proper
24 anti-ballistic air bag protection. These materials can be sewn or
25 configured in many ways to accommodate ballistic protection

1 applications; in the present invention, the selected material is
2 formed into air bags similar to those found in automobiles, but of
3 larger size and thickness. The strength to weight ratio of these
4 anti-ballistic fabrics are among the highest available, either man-
5 made or natural.

6 Turning now to Fig. 3, a three-view depiction of the deployed
7 air bag (25) of the present invention can be seen. After detection
8 and confirmation of a concussive shock wave or ballistic
9 projectile, an activation signal is sent to gas generator (210) so
10 that air bag (25) is inflated within approximately 20-30 msec of
11 receipt. Enclosure (20) has frangible upper surface (260) through
12 which air bag (25) emerges when inflated by gas generator (210).
13 Front surface (220), rear surface (230), and top surface (245) of
14 air bag (25) are made from SPECTRA®, KEVLAR®, or other similar
15 ultra-high molecular weight polyethylene fabric. Using such
16 construction results in a type of spaced-plate armor system. That
17 is, for a given level of protection, such a multi-plate system
18 results in a lighter protective element, per unit area, than using
19 a single, equivalent layer of the same material.

20 The inflation of air bag (25) by way of gas generator (210) is
21 also controlled using vents (240) and cross-ties (200). Air bag
22 (25) should optimally be configured to remain effectively inflated
23 and in place for at least two seconds.

24 The effectiveness of the anti-ballistic air bag (25) in
25 stopping a bullet is a function of the thicknesses of the front

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1 surface (220) and rear surface (230), as well as the distance
2 between them. The mechanical advantage of this spaced-plate system
3 lies in the fact that the front surface (220) slows, deforms, and
4 re-directs the projectile as it passes through; the slower,
5 tumbling projectile is then either halted or further re-directed by
6 the rear surface (230) of air bag (25).

7 In the present invention, any material of sufficient strength
8 and toughness to significantly re-direct a ballistic projectile
9 along its initial trajectory can be used to construct the air bag
10 (25). However, the preferred embodiment of air bag (25) is
11 constructed from SPECTRA®, due to its strength, ballistic
12 protection properties, and the ease with which it can be used to
13 fabricate the air bag (25). The thickness of the anti-ballistic
14 fabric can be varied and should be chosen to match a particular
15 threat.

16 The shape and dimensions of inflated air bag (25) can be
17 modified to meet the required level of protection (e.g. projectile
18 size and velocity), along with area coverage requirements. As
19 shown, the inflated anti-ballistic air bag (25) has a pillow shape,
20 and would be sized to cover a typical doorway if used as
21 illustrated in Fig. 1B. That is, the dimensions would be roughly
22 4 ft. wide by 8 ft. high by 1-1/2 ft. thick at the widest portion.
23 Air bag (25) is continuously attached to a base plate (250),
24 located near the bottom of enclosure (20), and held in place with
25 a pinching bar (not shown) around the periphery of base plate

1 (250).

2 The seams of air bag (25) are sewn using SPECTRA® or other,
3 similar fibers, and the structure of air bag (25) is reinforced
4 using cross-ties (200), also of SPECTRA® or similar material so
5 that the air bag (25) deploys vertically, rather than billowing
6 horizontally. The size and position of cross-ties (200) are a
7 function of the size of air bag (25), the required inflation time,
8 and the size of the gas generator (210). Air bag (25) also
9 contains reinforced vents (240) that are sized to control the peak
10 pressure experienced during inflation of air bag (25) and
11 therefore, the peak stress applied to the material used to
12 fabricate air bag (25). Vents (240) located in top surface (245)
13 of air bag (25) also act to provide a downward force which acts
14 against base plate (250) due to vertical jetting of gas expelled
15 through vents (240).

16 While the system is described as being implemented with
17 SPECTRA® fabric, which is a trademark of the Allied Fibers Division
18 of Allied Signal, Inc., other materials may be used. SPECTRA®
19 fiber is an ultra-high molecular weight polyethylene fiber with
20 high strength and low specific gravity. KEVLAR®, which is a
21 trademark for aramid fiber sold by DuPont, or Dyneema™ can also be
22 used. Also, such materials can be used in combination, such as
23 combining woven ballistic fabric and a non-woven SPECTRA® fiber
24 shield. This method is disclosed in U.S. Pat. No. 5,237,811 issued
25 to **Price, et al.** Any material which is described as an ultra-high

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1 molecular weight polyethylene fiber, or fabric, or any other
2 flexible material of sufficient strength to resist puncture by
3 typical bullet-like projectiles and concussive explosion blasts can
4 be used to implement the air bag of the instant invention.

5 Gas generator (210) is similar to that found in conventional
6 automobiles, but larger in size and utilizing a faster burning
7 oxidizer component. As illustrated in Fig. 3, a single gas
8 generator (210) is used. However, multiple generators (210) can be
9 used to reduce inflation time and prolong the duration of time
10 during which air bag (25) remains effectively deployed. Gas
11 generator (210) is affixed to base plate (250) and is surrounded by
12 insulation (215) which provides a thermal barrier between gas
13 generator (210), and the nearby base plate (250) and air bag (25).

14 Turning now to Fig. 4, a schematic block diagram of the
15 present invention, using a bi-static radar detection system for
16 ballistic projectiles, can be seen. In this embodiment of the
17 invention, an analog signal processing system is illustrated,
18 however, a RISC processor or other relatively fast digital computer
19 can also be used to process signals from sensory components in the
20 system to reliably detect the presence of a ballistic projectile or
21 concussive wave front

22 Power supply (305) is used to supply power to all components
23 employed in the detection, discrimination, and gas generator
24 activation circuits. In this particular embodiment, signal
25 generator (310) supplies a 10.5 GHz signal (normally continuous

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1 wave, but modulation for anti-jamming and noise rejection may be
2 added) to directional coupler (320). The generator signal is then
3 amplified by amplifier (330) and passed to transmitting antenna
4 (340) for illumination of incoming objects. The transmitted signal
5 is applied to the general area surrounding personnel to be
6 protected. Transmitting antennae (340) are operated with
7 approximately 100 milliwatts of power at a frequency of 10.5 GHz.
8 Dedicated receiving antenna (350) is passive. The bi-static
9 system, using a separate transmitting antenna (340) and receiving
10 antenna (350), provides greater received signal isolation and
11 greater detection range by reducing receiver signal overload (due
12 to spatial isolation between the respective antennae). Such a
13 system also provides greater flexibility in shaping detection
14 elevation and azimuth coverage. Receiving antenna (350) output is
15 amplified by low noise amplifier (360) and mixed with a sample of
16 the signal provided by signal generator (310) via directional
17 coupler (320) and mixer (370). The resulting signal, introduced
18 into broadband transformer (380) (North Hill Electronics, Inc.
19 model 0016PA, or equivalent), is a Doppler-shifted beat signal.
20 After passing the beat signal through high pass filter (390)
21 (optimally operating at a 3 dB point of 6 kHz, with maximum
22 rejection of 100 dB at 2 kHz), the signal is then amplified via
23 received signal amplifier (400), further filtered by way of low
24 pass filter (410) (optimally acting at a 3 dB point of 200 kHz,
25 maximum rejection of 100 dB at 600 kHz), further amplified using

1 signal amplifier (420), and passed on to tone decoder (430). The
2 low noise amplifier (360) should have as low a noise figure as
3 practical without being overly sensitive to in-band intermodulation
4 products. The broadband transformer (380) is not essential to
5 system functionality, but is useful for isolating ground-induced
6 noise and further limiting the received signal bandwidth to the
7 bands of interest. The signal amplifier (400) is a low noise (S/N
8 < 4 dB) amplifier operating at the doppler frequencies (20 to
9 70kHz). Performance is not critical to the operation of the
10 circuit as long as it provides enough gain with the received signal
11 amplifier (420) to trigger the tone decoder.

12 Tone decoder (430) responds to a Doppler shift produced by
13 predetermined bullet velocities. The shift is determined by the
14 well known equation $\Delta f = 2Vf_c/C$, where Δf is the doppler shift, V
15 is the velocity, f_c is the CW frequency, and C is the speed of
16 light. The tone decoders can be set for a nominal center frequency
17 and bandwidth (bandwidth should be limited to 14% of f_c). The
18 circuit values illustrated in Fig. 5 produce a response frequency
19 which corresponds to the velocity of a 9mm bullet. Tone decoder
20 response time varies with the velocity of the bullet plus many
21 other factors. Another detection method requires designing of a
22 recognition algorithm combined with digital signal processing of
23 the sampled doppler waveform. Much better sensitivity and lower
24 false alarms should be possible than those methods using simple
25 tone decoders, which function adequately and provide a lower cost

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1 approach. Multiple tone decoders (430) (not shown) with
2 overlapping frequency bands can also be used to detect a range of
3 Doppler shift frequencies so that a corresponding range of
4 ballistic projectile velocities can also be detected.

5 The ballistic protection embodiment of the present invention
6 may be refined by using one or more transmit and receive antennas
7 to produce a Doppler shift from ballistic projectiles entering a
8 well-defined volume of space. Such antennae combinations would be
9 placed in a specific series of locations optimized for ranging and
10 simultaneously reducing the chance of false alarms by signal
11 sources outside the radar field of view.

12 To overcome jamming which disables destructive force
13 detection, or deliberate activation of the system through use of
14 electromagnetic signals (either spurious or intended), anti-jamming
15 circuitry is also included in the present invention. Various
16 approaches are available, including signal amplitude and frequency
17 coding, as is well known to those skilled in the art. Such coding
18 may include simple sinusoidal amplitude or frequency modulation,
19 which in turn would produce recognizable side bands on a true
20 Doppler-shifted signal; such side bands would not appear as the
21 result of a jamming signal. More sophisticated coding techniques,
22 including signal doping, can also be used, but should be evaluated
23 in light of possible additional inflation signal output delays, as
24 derived from the resulting decoding constraints.

25 In other embodiments of the system, a RISC-type control

1 processor, or other fast signal processors as are known in the art,
2 may be used to conduct analysis of signals from receiving antenna
3 (350) after such signals have been suitably filtered and digitized.
4 Software may be used to do simple frequency detection. In
5 addition, algorithms may be used to recognize specific signals for
6 verification of frequency, amplitude, modulation, and/or spectral
7 content of the acquired signal. Redundant hardware and/or
8 processing algorithms can also be used to confirm the presence of
9 a ballistic projectile or concussive wave front, to minimize the
10 likelihood of accidental deployment.

11 Once the presence of a ballistic projectile has been reliably
12 detected, then the firing circuit (440) is activated. The squib
13 (450) (not shown) is located inside gas generator (210) and is used
14 to ignite the oxidizer therein. The gas generator (or gas
15 generators, since multiple units may be used, depending upon the
16 application) is a Primex 28534-301 (or equivalent) with 68 ft³ free
17 volume and approximately 1 lb of propellant. The generator is
18 initiated with a squib, such as an M-102 Atlas Match squib (or
19 equivalent) typically using a firing signal of 3 amps or more at 12
20 volts for a duration of 2 ms or longer.

21 Tone decoder (430) can be constructed from a conventional
22 LM567C tone decoder integrated circuit, or similar device, and is
23 used to detect the presence of certain frequencies to determine the
24 presence of a Doppler-shifted ballistic projectile signal.

25 Turning now to Fig. 5, the circuit diagram for tone decoder

(430) is illustrated. As can be seen, tone decoder integrated circuit (460) of type LM567C, or similar, is surrounded by conventional components, the particular values of which are illustrated on the diagram. Individual component values are determined by formulas well-known in the art, and the values shown in the figure are typical for detection of a Doppler-shifted frequency generated by a 9mm bullet. For example, it has been experimentally determined that the range of doppler shift varies from approximately 19 KHz to 26 kHz for a 9mm bullet travelling at speeds of 900 fps to 1200 fps, respectively. For a 5.56 mm bullet, the shift goes from 64 kHz to 73 kHz for velocities ranging from 3,000 fps to 3,400 fps, respectively. Of course, multiple tone decoders, operating simultaneously, can be used in this particular embodiment of the present invention, any one of which is capable of activating firing circuit (440).

Turning now to Fig. 6, a schematic diagram of the gas generator squib ignition circuitry is illustrated, using typical component values well known in the art. Generally, a signal of at least 3 amps at 12 volts must be present for a duration of 2 ms or longer. The propagation delay involved in firing the squib after receiving the validated concussive shock wave or ballistic projectile detection signal is approximately one msec, depending on tone decoder detection time.

Although the invention has been described with reference to specific embodiments, this description is not meant to be construed

